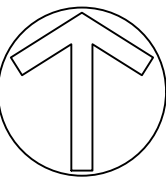
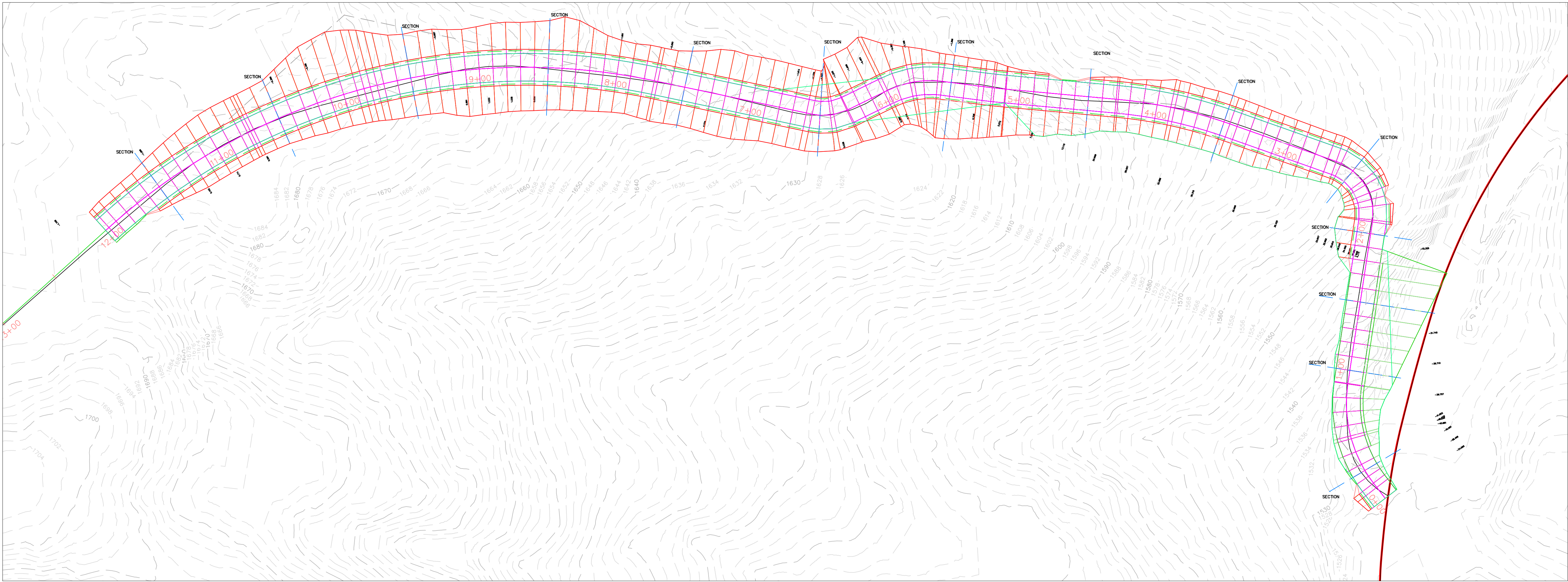






Drawing2.dwg

3/19/2007



3111 Carriker Lane  
Soquel, Ca 95073  
831-295-7631  
www.delveengineering.com

REVISIONS:

| REVISIONS | DATE | INT. |
|-----------|------|------|
| FIRST     |      |      |
| SECOND    |      |      |
| THIRD     |      |      |
| FOURTH    |      |      |

SCALE:

1" = 40'

DRAWN BY:

RSS

DESIGNED BY:

RSS

CHECKED BY:

DATE:

APPROVED BY:

DATE:

TITLE:

LAKE CO DEVELOPMENT  
VARIOUS APN'S  
LAKE COUNTY, CA

ROADWAY IMPROVEMENTS

EXHIBIT

DATE:

05/08/2021

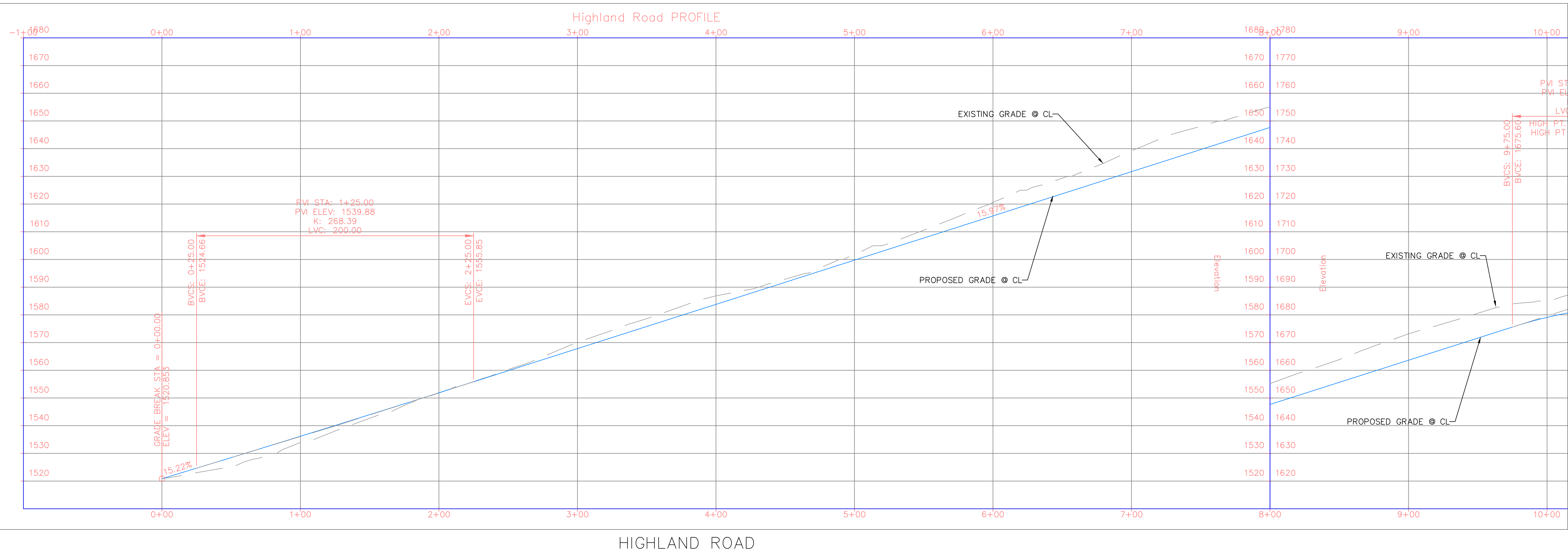
PROJECT ID:

2021\_009

DRAWING NO.:

C-1

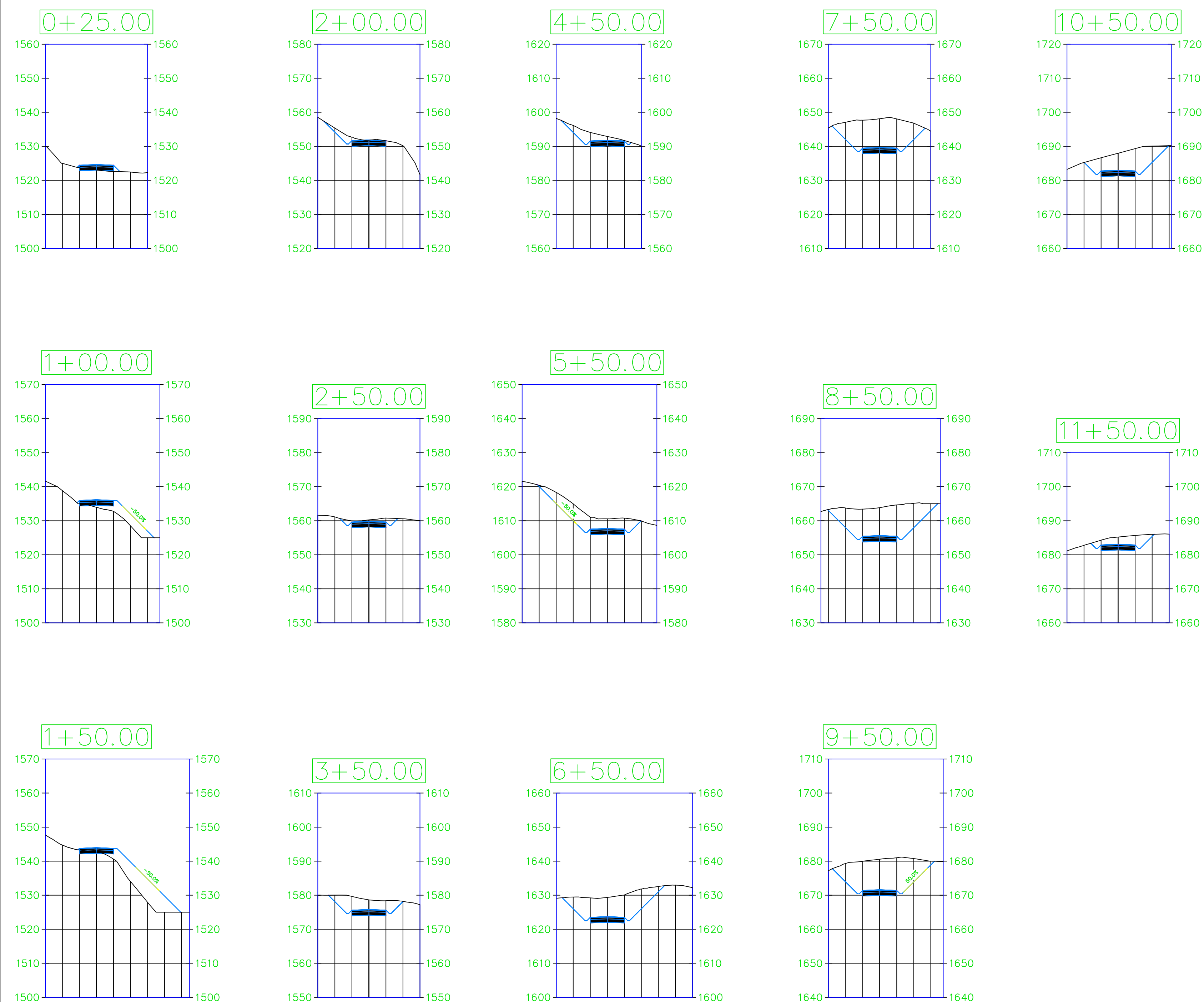
SHT 1 OF 3











Cut/Fill Report

Generated:

2021-05-13 16:0140

By user:

Rider2

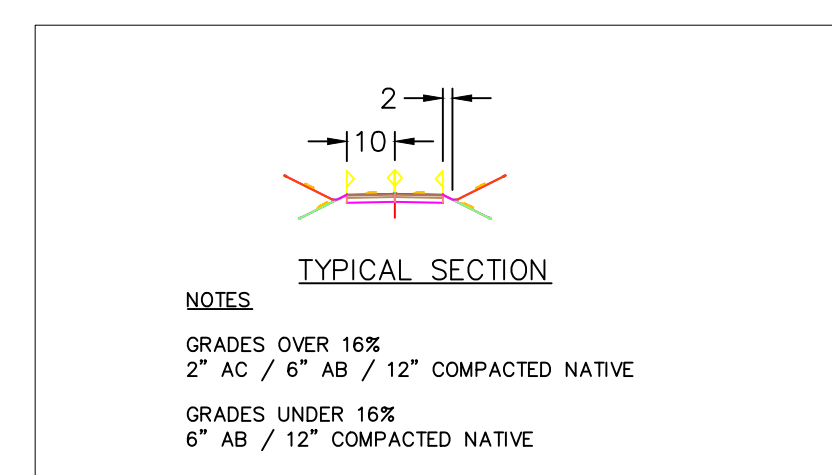
Drawing:

D:\WORK\PROJECTS\2021\_009 Lake County GIS\2\_Planning\4\_CAD Doc\I\WORK\PROJECTS\2021\_009 Lake County GIS\2\_Planning\4\_CAD Doc\Drawing2.dwg

Volume Summary

| Name                   | Type | Cut Factor | Fill Factor | 2d Area<br>(Sq. Ft.) | Cut<br>(Cu. Yd.) | Fill<br>(Cu. Yd.) | Net<br>(Cu. Yd.) |
|------------------------|------|------------|-------------|----------------------|------------------|-------------------|------------------|
| Highland Road_cut&fill | full | 1.000      | 1.000       | 31740.54             | 6167.31          | 372.22            | 5795.09<Cut>     |
| Totals                 |      |            |             |                      |                  |                   |                  |
|                        |      |            |             | 31740.54             | 6167.31          | 372.22            | 5795.09<Cut>     |

\* Value adjusted by cut or fill factor other than 1



HIGHLAND ROAD





#1 - 18.5 cfs 36" / water depth less than 24"  
38.940370 -122.921945  
(cut) 8,880cy (fill) 8,880cy (net) 0cy

#2 - 1.5 cfs 12" with water depth less than 9"  
38.940187 -122.920507  
(cut) 48cy (fill) 48cy (net) 0cy

#3 - 2.5 cfs ` 18" with water depth less than 11"  
38.941485 -122.918850  
(cut) 45cy (fill) 45cy (net) 0cy

#4 - 3.3 cfs 18" with water depth less than 12"  
38.942293 -122.918027  
(cut) 27cy (fill) 27cy (net) 0cy



# THE McEDWARDS GROUP

14054 Sugar Loaf Road  
Grass Valley CA 95949  
License #743428

Phone: (707) 354-4618

themcedwardsgroup@att.net

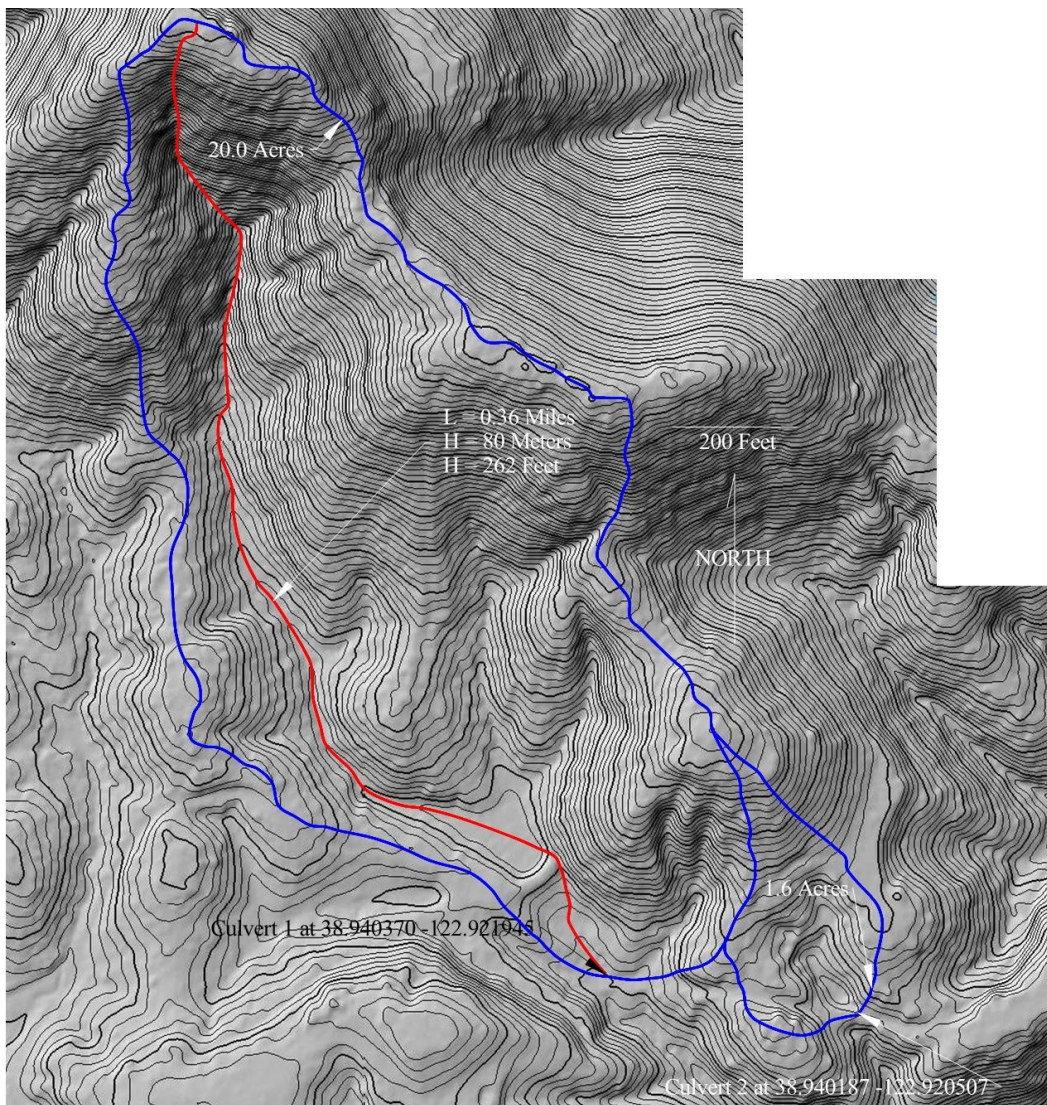
September 24, 2021  
Job No. 2107.02.01

Joseph Cooper  
7525 Highland Springs Road  
Lakeport, CA 95453

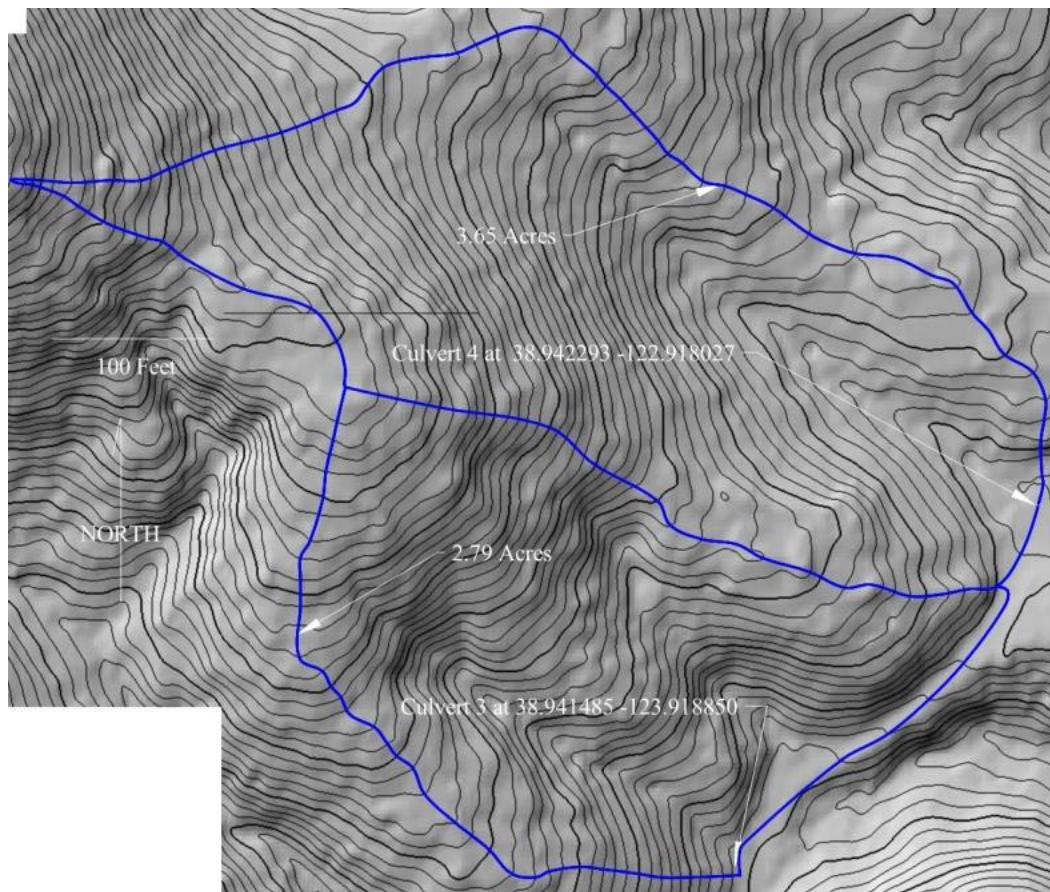
100 Year Storm Culvert Sizing  
Culverts 1 through 4  
7525 Highland Springs Road  
Lakeport, California

Dear Mr. Cooper,

This report describes the procedure, and results thereof, that we used to determine the diameter of four road culverts (designated at Culverts 1 through 4) at your Lakeport property to convey runoff generated by a 100-year return-interval storm. The numbered culvert locations and their watershed areas are shown on the 1 meter contour interval maps below that were obtained from <https://apps.nationalmap.gov/3depdem/>.







To determine the flowrate of a 100-year storm at the culvert location, we used the Rational Method described in the CalFire document *Designing Watercourse Crossings for Passage of 100-Year Flood Flows, Wood, and Sediment (Updated 2017)* found at [http://calfire.ca.gov/resource\\_mgmt/downloads/100%20yr%20revised%2008-08-17%20\(final-a\).pdf](http://calfire.ca.gov/resource_mgmt/downloads/100%20yr%20revised%2008-08-17%20(final-a).pdf) and referenced in SWRCB Order WQ 2017-0023-DWQ.

The rational method formulae is  $Q = ciA$  where  $Q$  is the flowrate in cubic feet per second (cfs),  $c$  is a runoff coefficient (fraction of rainfall that becomes runoff),  $i$  is rainfall intensity in inches per hour, and  $A$  is the contributing watershed area in acres. The intensity of rainfall depends of the time of concentration  $T_c$ , the time it takes for runoff from the farthest point in the watershed to reach the culvert. According to the California Culvert Practice formulae, which formula is presented in the CalFire document,  $T_c$  depends on both the length ( $L$ ) of the runoff path from the farthest point to the culvert, and the elevation difference ( $H$ ) between the farthest point and the culvert as  $T_c = (11.9 * L^3 / H)^{0.385}$ , where  $L$  is in miles,  $H$  is in feet, and  $T_c$  is in hours.  $A$ ,  $L$ , and  $H$  were measured for the Culvert 1 watershed, and these values gave a  $T_c$  of less than six minutes. Because the CalFire document recommends using a  $T_c$  of 10 minutes when the calculated  $T_c$  is less than 10 minutes, we used the rainfall intensity for a time of concentration of 10 minutes for the Culvert 1 watershed and for the smaller watersheds of Culverts 2, 3, and 4.

The GPS coordinates of the culvert crossings are given below.

|           |           |             |           |           |             |
|-----------|-----------|-------------|-----------|-----------|-------------|
| Culvert 1 | 38.940370 | -122.921945 | Culvert 3 | 38.941485 | -122.918850 |
| Culvert 2 | 38.940187 | -122.920507 | Culvert 4 | 38.942293 | -122.918027 |

With these coordinates, we used NOAA's National Weather Service Hydrometrological Design Center Precipitation Frequency Data Server (PFDS) found at <https://hdsc.nws.noaa.gov/hdsc/pfds> to determine the rainfall intensity at the location of the culverts for a time of concentration of 10 minutes. The Point Precipitation Frequency Estimates data tables obtained from the NOAA server are attached. With  $i$  known, the 100-year flows for each culvert crossing were calculated. Using these flows with the Headwater Depth for C. M. Pipe Culverts with Inlet Control nomograph provided in the CalFire document, we determined the appropriate culvert sizes to handle the flows. The calculation of 100-year flows is shown on the attached spreadsheet. The determination of the culvert sizes to carry the calculated 100-year flows is shown on the attached Inlet Control nomograph.



The 100-year flows and required culverts sizes for each culvert crossing are given below.

| Culvert No. | 100-Year Storm Flow | Required CMP Culvert Diameter      |
|-------------|---------------------|------------------------------------|
| 1           | 18.5 cfs            | 36" with water depth less than 24" |
| 2           | 1.5                 | 12" with water depth less than 9"  |
| 3           | 2.5                 | 18" with water depth less than 11" |
| 4           | 3.3                 | 18" with water depth less than 12" |

We appreciate the opportunity to be of service. If you have any questions, please call.

Very Truly Yours,

THE MCEDWARDS GROUP

|                                                                                                                                                  |                                                                                                                                                                        |                                                                                   |
|--------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|
| <small>STATE OF CALIFORNIA</small><br><b>dca</b><br><small>DEPARTMENT OF CONSUMER AFFAIRS</small>                                                | <small>BOARD FOR PROFESSIONAL ENGINEERS,<br/>LAND SURVEYORS, AND GEOLOGISTS</small><br>2535 CAPITOL OAKS DRIVE, SUITE 300<br>SACRAMENTO, CA 95833-2944<br>916 263-2222 |  |
| <b>CERTIFIED<br/>HYDROGEOLOGIST</b>                                                                                                              |                                                                                                                                                                        | <small>EXPIRATION</small><br><b>06/30/21</b>                                      |
| <small>CERTIFICATE NO.</small><br><b>HG 153</b><br><b>DONALD GEORGE MC EDWARDS</b><br><b>14054 SUGAR LOAF RD</b><br><b>GRASS VALLEY CA 95949</b> |                                                                                                                                                                        |                                                                                   |
| <small>Signature</small> <u>Donald G. McEdwards</u>                                                                                              | <small>RECEIPT NO.</small><br>91130028                                                                                                                                 |                                                                                   |

Dr. Donald G. McEdwards, CE 28088, HG 153

Attachments: Point precipitation frequency estimates  
Rational method spreadsheet  
Headwater Depth for C. M. Pipe Culverts with Inlet Control Nomograph





### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps\\_&\\_aerials](#)

Culvert 1

### PF tabular

| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup> |                                     |                        |                        |                        |                        |                        |                        |                        |                        |                        |
|----------------------------------------------------------------------------------------------------------|-------------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| Duration                                                                                                 | Average recurrence interval (years) |                        |                        |                        |                        |                        |                        |                        |                        |                        |
|                                                                                                          | 1                                   | 2                      | 5                      | 10                     | 25                     | 50                     | 100                    | 200                    | 500                    | 1000                   |
| 5-min                                                                                                    | 0.130<br>(0.116-0.148)              | 0.159<br>(0.141-0.181) | 0.198<br>(0.175-0.226) | 0.231<br>(0.203-0.267) | 0.279<br>(0.235-0.335) | 0.318<br>(0.261-0.390) | 0.358<br>(0.286-0.453) | 0.403<br>(0.312-0.526) | 0.466<br>(0.344-0.639) | 0.519<br>(0.368-0.739) |
| 10-min                                                                                                   | 0.187<br>(0.166-0.212)              | 0.228<br>(0.202-0.259) | 0.284<br>(0.251-0.324) | 0.332<br>(0.291-0.383) | 0.400<br>(0.337-0.480) | 0.455<br>(0.374-0.559) | 0.514<br>(0.410-0.650) | 0.577<br>(0.447-0.754) | 0.668<br>(0.493-0.916) | 0.744<br>(0.527-1.06)  |
| 15-min                                                                                                   | 0.226<br>(0.201-0.257)              | 0.275<br>(0.244-0.314) | 0.343<br>(0.304-0.392) | 0.401<br>(0.351-0.463) | 0.484<br>(0.407-0.580) | 0.550<br>(0.452-0.677) | 0.621<br>(0.496-0.786) | 0.698<br>(0.540-0.912) | 0.808<br>(0.596-1.11)  | 0.899<br>(0.638-1.28)  |
| 30-min                                                                                                   | 0.317<br>(0.281-0.360)              | 0.386<br>(0.343-0.440) | 0.482<br>(0.426-0.550) | 0.563<br>(0.493-0.649) | 0.679<br>(0.572-0.814) | 0.772<br>(0.635-0.949) | 0.872<br>(0.697-1.10)  | 0.980<br>(0.758-1.28)  | 1.13<br>(0.836-1.55)   | 1.26<br>(0.895-1.80)   |
| 60-min                                                                                                   | 0.448<br>(0.398-0.509)              | 0.546<br>(0.484-0.622) | 0.681<br>(0.602-0.778) | 0.795<br>(0.697-0.918) | 0.959<br>(0.808-1.15)  | 1.09<br>(0.897-1.34)   | 1.23<br>(0.984-1.56)   | 1.38<br>(1.07-1.81)    | 1.60<br>(1.18-2.19)    | 1.78<br>(1.26-2.54)    |
| 2-hr                                                                                                     | 0.698<br>(0.620-0.793)              | 0.852<br>(0.756-0.970) | 1.06<br>(0.933-1.21)   | 1.22<br>(1.07-1.41)    | 1.45<br>(1.22-1.74)    | 1.63<br>(1.34-2.00)    | 1.81<br>(1.45-2.29)    | 2.00<br>(1.55-2.62)    | 2.27<br>(1.67-3.10)    | 2.47<br>(1.75-3.53)    |
| 3-hr                                                                                                     | 0.917<br>(0.814-1.04)               | 1.12<br>(0.993-1.27)   | 1.38<br>(1.22-1.58)    | 1.59<br>(1.40-1.84)    | 1.88<br>(1.58-2.26)    | 2.10<br>(1.72-2.58)    | 2.32<br>(1.85-2.93)    | 2.55<br>(1.97-3.32)    | 2.85<br>(2.10-3.91)    | 3.09<br>(2.19-4.41)    |
| 6-hr                                                                                                     | 1.43<br>(1.27-1.63)                 | 1.75<br>(1.56-2.00)    | 2.16<br>(1.91-2.47)    | 2.49<br>(2.18-2.87)    | 2.92<br>(2.46-3.50)    | 3.24<br>(2.66-3.98)    | 3.55<br>(2.84-4.49)    | 3.87<br>(3.00-5.06)    | 4.29<br>(3.17-5.88)    | 4.61<br>(3.27-6.58)    |
| 12-hr                                                                                                    | 2.12<br>(1.88-2.41)                 | 2.66<br>(2.36-3.03)    | 3.34<br>(2.95-3.81)    | 3.87<br>(3.39-4.46)    | 4.55<br>(3.84-5.46)    | 5.06<br>(4.16-6.22)    | 5.56<br>(4.44-7.02)    | 6.05<br>(4.68-7.90)    | 6.69<br>(4.93-9.16)    | 7.17<br>(5.08-10.2)    |
| 24-hr                                                                                                    | 3.05<br>(2.74-3.47)                 | 3.94<br>(3.53-4.48)    | 5.04<br>(4.51-5.74)    | 5.89<br>(5.24-6.76)    | 6.99<br>(6.04-8.26)    | 7.80<br>(6.61-9.38)    | 8.58<br>(7.12-10.5)    | 9.36<br>(7.58-11.8)    | 10.4<br>(8.10-13.5)    | 11.1<br>(8.42-14.9)    |
| 2-day                                                                                                    | 4.08<br>(3.67-4.64)                 | 5.26<br>(4.71-5.98)    | 6.71<br>(6.01-7.65)    | 7.85<br>(6.97-9.01)    | 9.31<br>(8.04-11.0)    | 10.4<br>(8.80-12.5)    | 11.4<br>(9.48-14.0)    | 12.4<br>(10.1-15.7)    | 13.8<br>(10.8-18.0)    | 14.8<br>(11.2-19.9)    |
| 3-day                                                                                                    | 4.76<br>(4.27-5.41)                 | 6.10<br>(5.47-6.94)    | 7.78<br>(6.96-8.87)    | 9.08<br>(8.07-10.4)    | 10.8<br>(9.30-12.7)    | 12.0<br>(10.2-14.4)    | 13.2<br>(11.0-16.2)    | 14.4<br>(11.7-18.1)    | 15.9<br>(12.5-20.8)    | 17.1<br>(12.9-23.0)    |
| 4-day                                                                                                    | 5.30<br>(4.76-6.03)                 | 6.80<br>(6.10-7.73)    | 8.65<br>(7.74-9.87)    | 10.1<br>(8.97-11.6)    | 12.0<br>(10.3-14.1)    | 13.3<br>(11.3-16.0)    | 14.7<br>(12.2-18.0)    | 16.0<br>(12.9-20.1)    | 17.7<br>(13.8-23.1)    | 18.9<br>(14.4-25.5)    |
| 7-day                                                                                                    | 6.55<br>(5.88-7.44)                 | 8.38<br>(7.51-9.53)    | 10.6<br>(9.52-12.1)    | 12.4<br>(11.0-14.2)    | 14.6<br>(12.6-17.3)    | 16.3<br>(13.8-19.6)    | 17.9<br>(14.9-22.0)    | 19.5<br>(15.8-24.5)    | 21.5<br>(16.8-28.1)    | 23.0<br>(17.4-30.9)    |
| 10-day                                                                                                   | 7.48<br>(6.71-8.49)                 | 9.55<br>(8.57-10.9)    | 12.1<br>(10.8-13.8)    | 14.1<br>(12.5-16.2)    | 16.6<br>(14.4-19.7)    | 18.5<br>(15.7-22.2)    | 20.3<br>(16.8-24.9)    | 22.0<br>(17.8-27.7)    | 24.3<br>(19.0-31.7)    | 25.9<br>(19.7-34.9)    |
| 20-day                                                                                                   | 9.89<br>(8.88-11.2)                 | 12.6<br>(11.3-14.4)    | 16.0<br>(14.3-18.3)    | 18.6<br>(16.5-21.3)    | 21.9<br>(18.9-25.8)    | 24.2<br>(20.5-29.1)    | 26.5<br>(22.0-32.5)    | 28.7<br>(23.2-36.1)    | 31.5<br>(24.6-41.1)    | 33.5<br>(25.4-45.1)    |
| 30-day                                                                                                   | 12.0<br>(10.7-13.6)                 | 15.3<br>(13.7-17.4)    | 19.3<br>(17.3-22.0)    | 22.3<br>(19.8-25.6)    | 26.2<br>(22.6-30.9)    | 28.9<br>(24.5-34.8)    | 31.5<br>(26.2-38.8)    | 34.1<br>(27.6-42.9)    | 37.3<br>(29.2-48.7)    | 39.7<br>(30.1-53.4)    |
| 45-day                                                                                                   | 14.8<br>(13.3-16.9)                 | 18.9<br>(16.9-21.4)    | 23.7<br>(21.2-27.0)    | 27.3<br>(24.3-31.4)    | 31.9<br>(27.5-37.7)    | 35.1<br>(29.8-42.2)    | 38.2<br>(31.7-46.9)    | 41.1<br>(33.3-51.8)    | 44.8<br>(35.0-58.5)    | 47.5<br>(36.0-63.9)    |
| 60-day                                                                                                   | 17.5<br>(15.7-19.8)                 | 22.0<br>(19.8-25.1)    | 27.5<br>(24.6-31.4)    | 31.6<br>(28.1-36.3)    | 36.7<br>(31.7-43.4)    | 40.3<br>(34.2-48.5)    | 43.7<br>(36.3-53.7)    | 47.0<br>(38.1-59.2)    | 51.1<br>(39.9-66.7)    | 54.0<br>(40.9-72.7)    |

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not





### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps\\_&\\_aerials](#)

Culverts 2, 3, and 4

### PF tabular

| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup> |                                     |                        |                        |                        |                        |                        |                        |                        |                        |                        |
|----------------------------------------------------------------------------------------------------------|-------------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| Duration                                                                                                 | Average recurrence interval (years) |                        |                        |                        |                        |                        |                        |                        |                        |                        |
|                                                                                                          | 1                                   | 2                      | 5                      | 10                     | 25                     | 50                     | 100                    | 200                    | 500                    | 1000                   |
| 5-min                                                                                                    | 0.128<br>(0.113-0.145)              | 0.156<br>(0.138-0.178) | 0.194<br>(0.172-0.222) | 0.227<br>(0.199-0.262) | 0.274<br>(0.231-0.329) | 0.312<br>(0.257-0.384) | 0.352<br>(0.282-0.446) | 0.396<br>(0.306-0.517) | 0.459<br>(0.338-0.628) | 0.510<br>(0.362-0.727) |
| 10-min                                                                                                   | 0.183<br>(0.163-0.208)              | 0.223<br>(0.198-0.254) | 0.279<br>(0.246-0.318) | 0.326<br>(0.285-0.376) | 0.393<br>(0.331-0.471) | 0.447<br>(0.368-0.550) | 0.505<br>(0.404-0.639) | 0.568<br>(0.439-0.741) | 0.657<br>(0.485-0.900) | 0.731<br>(0.518-1.04)  |
| 15-min                                                                                                   | 0.221<br>(0.197-0.252)              | 0.270<br>(0.240-0.308) | 0.337<br>(0.298-0.385) | 0.394<br>(0.345-0.455) | 0.475<br>(0.400-0.570) | 0.541<br>(0.445-0.665) | 0.611<br>(0.488-0.772) | 0.687<br>(0.531-0.896) | 0.795<br>(0.586-1.09)  | 0.884<br>(0.627-1.26)  |
| 30-min                                                                                                   | 0.311<br>(0.276-0.354)              | 0.380<br>(0.337-0.432) | 0.474<br>(0.419-0.541) | 0.554<br>(0.485-0.639) | 0.668<br>(0.562-0.801) | 0.760<br>(0.625-0.934) | 0.858<br>(0.686-1.09)  | 0.965<br>(0.746-1.26)  | 1.12<br>(0.824-1.53)   | 1.24<br>(0.881-1.77)   |
| 60-min                                                                                                   | 0.439<br>(0.390-0.500)              | 0.536<br>(0.475-0.611) | 0.669<br>(0.591-0.764) | 0.782<br>(0.685-0.902) | 0.943<br>(0.794-1.13)  | 1.07<br>(0.882-1.32)   | 1.21<br>(0.968-1.53)   | 1.36<br>(1.05-1.78)    | 1.58<br>(1.16-2.16)    | 1.75<br>(1.24-2.50)    |
| 2-hr                                                                                                     | 0.684<br>(0.607-0.778)              | 0.836<br>(0.741-0.952) | 1.04<br>(0.916-1.18)   | 1.20<br>(1.05-1.39)    | 1.43<br>(1.20-1.71)    | 1.60<br>(1.32-1.97)    | 1.78<br>(1.42-2.25)    | 1.97<br>(1.52-2.57)    | 2.23<br>(1.64-3.05)    | 2.43<br>(1.72-3.46)    |
| 3-hr                                                                                                     | 0.899<br>(0.798-1.02)               | 1.10<br>(0.974-1.25)   | 1.36<br>(1.20-1.55)    | 1.57<br>(1.37-1.81)    | 1.85<br>(1.56-2.21)    | 2.06<br>(1.69-2.53)    | 2.28<br>(1.82-2.88)    | 2.50<br>(1.93-3.26)    | 2.80<br>(2.07-3.84)    | 3.03<br>(2.15-4.32)    |
| 6-hr                                                                                                     | 1.40<br>(1.24-1.59)                 | 1.72<br>(1.52-1.96)    | 2.12<br>(1.87-2.42)    | 2.44<br>(2.13-2.81)    | 2.86<br>(2.41-3.43)    | 3.17<br>(2.61-3.90)    | 3.48<br>(2.78-4.40)    | 3.79<br>(2.93-4.95)    | 4.20<br>(3.10-5.76)    | 4.52<br>(3.20-6.43)    |
| 12-hr                                                                                                    | 2.07<br>(1.84-2.36)                 | 2.60<br>(2.31-2.96)    | 3.26<br>(2.88-3.73)    | 3.78<br>(3.31-4.36)    | 4.45<br>(3.75-5.34)    | 4.95<br>(4.07-6.08)    | 5.43<br>(4.34-6.86)    | 5.91<br>(4.57-7.72)    | 6.54<br>(4.82-8.95)    | 7.01<br>(4.97-9.98)    |
| 24-hr                                                                                                    | 2.99<br>(2.69-3.40)                 | 3.85<br>(3.45-4.38)    | 4.92<br>(4.40-5.61)    | 5.75<br>(5.11-6.60)    | 6.82<br>(5.89-8.06)    | 7.61<br>(6.45-9.15)    | 8.37<br>(6.95-10.3)    | 9.13<br>(7.40-11.5)    | 10.1<br>(7.90-13.2)    | 10.8<br>(8.22-14.6)    |
| 2-day                                                                                                    | 4.00<br>(3.59-4.54)                 | 5.14<br>(4.61-5.85)    | 6.56<br>(5.87-7.48)    | 7.67<br>(6.81-8.80)    | 9.09<br>(7.85-10.7)    | 10.1<br>(8.60-12.2)    | 11.2<br>(9.26-13.7)    | 12.2<br>(9.85-15.3)    | 13.5<br>(10.5-17.6)    | 14.4<br>(10.9-19.4)    |
| 3-day                                                                                                    | 4.65<br>(4.18-5.28)                 | 5.97<br>(5.35-6.79)    | 7.60<br>(6.80-8.67)    | 8.87<br>(7.89-10.2)    | 10.5<br>(9.09-12.4)    | 11.7<br>(9.95-14.1)    | 12.9<br>(10.7-15.9)    | 14.1<br>(11.4-17.7)    | 15.6<br>(12.2-20.3)    | 16.7<br>(12.6-22.4)    |
| 4-day                                                                                                    | 5.18<br>(4.65-5.89)                 | 6.64<br>(5.96-7.55)    | 8.45<br>(7.56-9.64)    | 9.86<br>(8.77-11.3)    | 11.7<br>(10.1-13.8)    | 13.0<br>(11.0-15.7)    | 14.3<br>(11.9-17.6)    | 15.6<br>(12.6-19.6)    | 17.3<br>(13.5-22.5)    | 18.5<br>(14.0-24.9)    |
| 7-day                                                                                                    | 6.40<br>(5.75-7.28)                 | 8.19<br>(7.34-9.31)    | 10.4<br>(9.30-11.9)    | 12.1<br>(10.8-13.9)    | 14.3<br>(12.4-16.9)    | 15.9<br>(13.5-19.2)    | 17.5<br>(14.5-21.5)    | 19.0<br>(15.4-23.9)    | 21.0<br>(16.4-27.4)    | 22.5<br>(17.0-30.2)    |
| 10-day                                                                                                   | 7.30<br>(6.56-8.30)                 | 9.33<br>(8.37-10.6)    | 11.8<br>(10.6-13.5)    | 13.8<br>(12.2-15.8)    | 16.2<br>(14.0-19.2)    | 18.0<br>(15.3-21.7)    | 19.8<br>(16.4-24.3)    | 21.5<br>(17.4-27.1)    | 23.7<br>(18.5-30.9)    | 25.3<br>(19.2-34.0)    |
| 20-day                                                                                                   | 9.66<br>(8.67-11.0)                 | 12.3<br>(11.1-14.0)    | 15.6<br>(14.0-17.8)    | 18.1<br>(16.1-20.8)    | 21.3<br>(18.4-25.2)    | 23.6<br>(20.0-28.4)    | 25.8<br>(21.5-31.8)    | 28.0<br>(22.7-35.2)    | 30.7<br>(24.0-40.1)    | 32.7<br>(24.8-44.0)    |
| 30-day                                                                                                   | 11.7<br>(10.5-13.3)                 | 14.9<br>(13.4-16.9)    | 18.8<br>(16.8-21.4)    | 21.8<br>(19.4-25.0)    | 25.5<br>(22.1-30.2)    | 28.2<br>(23.9-34.0)    | 30.8<br>(25.6-37.8)    | 33.3<br>(27.0-41.9)    | 36.4<br>(28.5-47.6)    | 38.7<br>(29.4-52.1)    |
| 45-day                                                                                                   | 14.5<br>(13.0-16.5)                 | 18.4<br>(16.5-20.9)    | 23.1<br>(20.7-26.3)    | 26.7<br>(23.7-30.6)    | 31.1<br>(26.9-36.8)    | 34.3<br>(29.1-41.2)    | 37.3<br>(30.9-45.8)    | 40.2<br>(32.5-50.6)    | 43.8<br>(34.2-57.2)    | 46.4<br>(35.2-62.4)    |
| 60-day                                                                                                   | 17.0<br>(15.3-19.4)                 | 21.5<br>(19.3-24.5)    | 26.9<br>(24.0-30.6)    | 30.9<br>(27.4-35.5)    | 35.9<br>(31.0-42.4)    | 39.4<br>(33.4-47.4)    | 42.7<br>(35.5-52.5)    | 45.9<br>(37.2-57.8)    | 49.9<br>(39.0-65.2)    | 52.8<br>(40.1-71.1)    |

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not



## RATIONAL METHOD SPREADSHEET

$$Q_{100} = CiA$$

$Q_{100}$  = predicted peak runoff from a 100-year storm (cubic feet per second, cfs)

$C$  = runoff coefficient

$i$  = rainfall intensity (inches per hour) for the 100-year storm

$A$  = basin drainage area (acres)

$i$  depends on the Time of Concentration,  $T_c$

$T_c = (11.9 \times L^3 / H)^{0.385}$  Kirpick Formula

$T_c$  = time of concentration (hours)

$L$  = length of the channel in miles from the head of the watershed to the crossing point

$H$  = elevation difference between the highest point in the watershed and the crossing point (feet)

Values for rational runoff coefficients (Dunne and Leopold 1978).

Woodland Soils in Rural Areas

Runoff Coefficient ( $C$ )

Sandy and gravelly soils

0.1

Loams and similar soils without impeding horizons

0.3

Heavy clay soils or those with a shallow impeding horizon; shallow soils over bedrock

0.4

Use 1 meter contour interval map of site (<https://apps.nationalmap.gov/3depdem/>) to determine watershed area

Use [hdsc.nws.noaa.gov/hdsc/pfds/](https://hdsc.nws.noaa.gov/hdsc/pfds/) with gps and  $T_c$  to determine  $i$  for 100 year storm

### Culvert 1

|          |            |           |              |
|----------|------------|-----------|--------------|
| Latitude | 38.940370  | Longitude | -122.921945  |
| $A =$    | 20 acres   |           |              |
| $H =$    | 262 feet   | $T_c =$   | 0.093 hours  |
| $L =$    | 0.36 miles |           | 5.61 minutes |
| $C =$    | 0.3        |           |              |

Because  $T_c$  is less than 10 minutes, use  $T_c = 10$  minutes as recommended by CalFire document for this and the other three smaller culvert watersheds

|                  |       |                    |                |              |     |
|------------------|-------|--------------------|----------------|--------------|-----|
| $T_c$ in Minutes | Depth |                    |                |              |     |
| 10               | 0.514 | inches in 10 min = | 0.051 in/min = | 3.08 in/hour |     |
|                  | $C$   | $i$                | $A$            | $= Q$        |     |
| $Q_{100} =$      | 0.30  | 3.08               | 20.00          | 18.5         | cfs |

From Nomograph: A 36" CMP culvert with a headwall entrance will pass 18.5 cfs with a water depth of less than 0.66 of pipe diameter or 24 inches



**Culvert 2**

Latitude 38.940187 Longitude -122.920507  
 A= 1.6 acres  
 C= 0.3

Tc in Minutes 10 Depth 0.505 inches in 10 min = 0.051 in/min = 3.03 in/hour

Q100 = C 0.30 i 3.03 A 1.60 = Q 1.5 cfs

From Nomograph: A 12" CMP culvert with a headwall entrance will pass 1.5 cfs with a water depth of less than 0.74 of pipe diameter or 9 inches

**Culvert 3**

Latitude 38.941485 Longitude -122.91885  
 A= 2.79 acres  
 C= 0.3

Tc in Minutes 10 Depth 0.505 inches in 10 min = 0.051 in/min = 3.03 in/hour

Q100 = C 0.30 i 3.03 A 2.79 = Q 2.5 cfs

From Nomograph: An 18" CMP culvert with a headwall entrance will pass 2.5 cfs with a water depth of less than 0.57 of pipe diameter or 11 inches

**Culvert 4**

Latitude 38.942293 Longitude -122.918027  
 A= 3.65 acres  
 C= 0.3

Tc in Minutes 10 Depth 0.505 inches in 10 min = 0.051 in/min = 3.03 in/hour

Q100 = C 0.30 i 3.03 A 3.65 = Q 3.3 cfs

From Nomograph: An 18" CMP culvert with a headwall entrance will pass 3.3 cfs with a water depth of less than 0.67 of pipe diameter or 12 inches



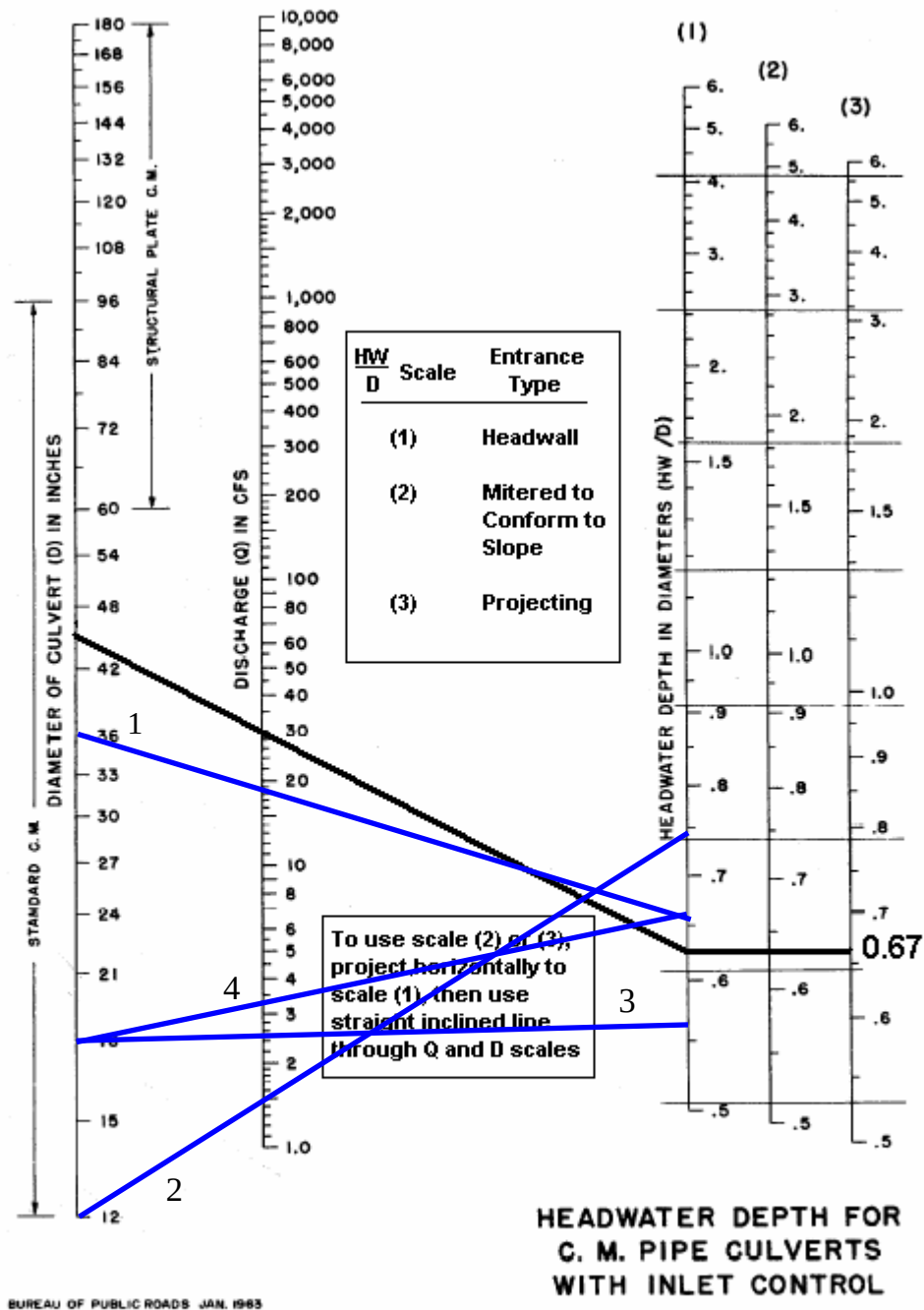
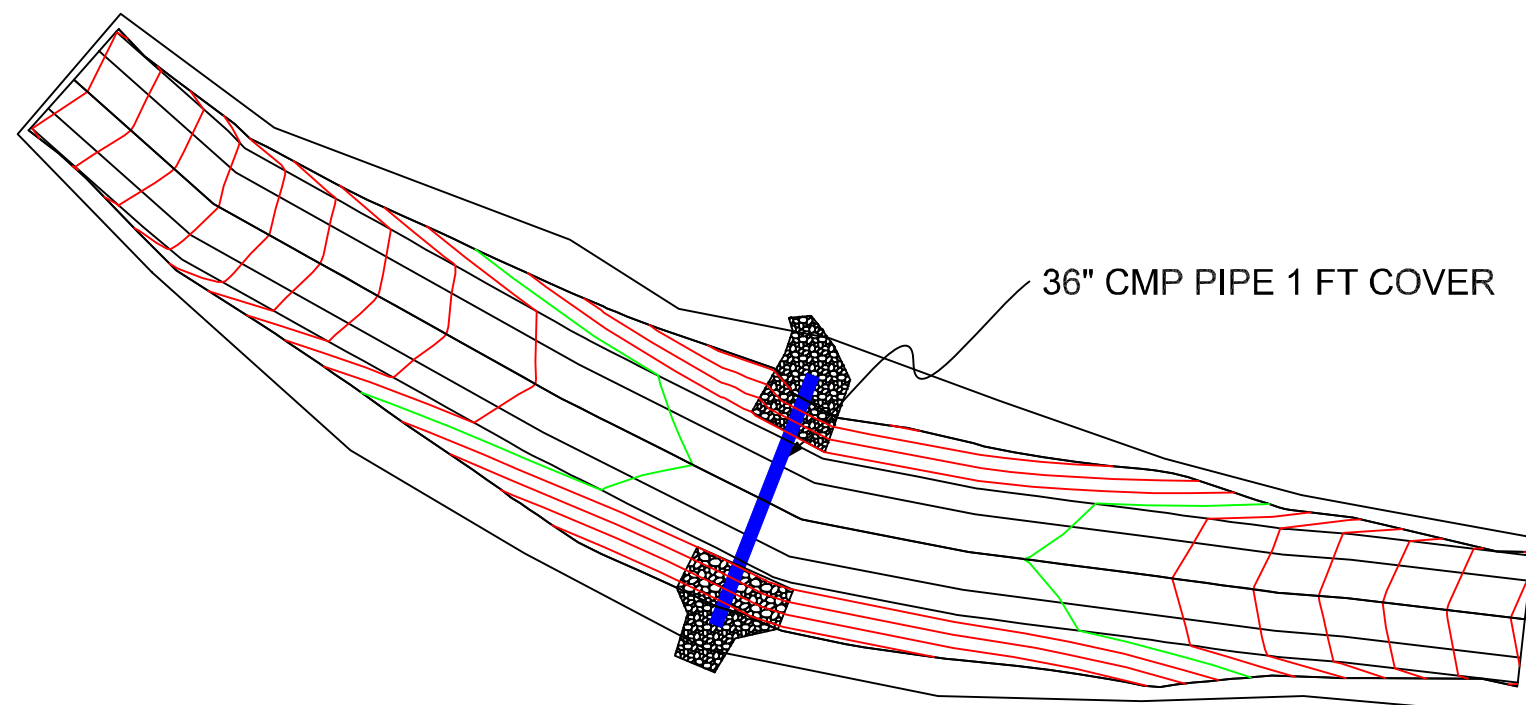
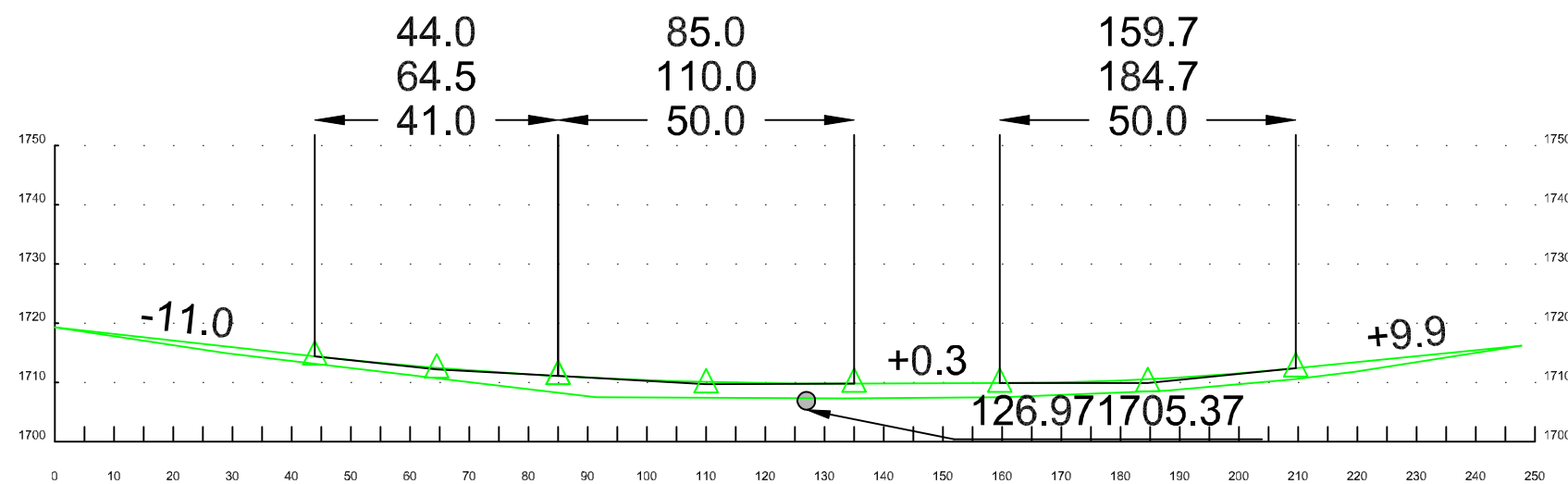


Figure 12. Normann and others (1985) culvert sizing nomograph for a round pipe with inlet control. For the watershed HEN example, using the direct transference method result of 30 cfs, a projecting pipe inlet, and a HW/D ratio of 0.67, the culvert size is 45 inches.





Tue Oct 26 08:59:48 2021



NTS

Processing 0+00.000 to 2+47.712  
 Total Fill: 237,622.4 C.F., 8,800.831 C.Y.  
 Cut to Fill Ratio: 0.00  
 Disturbed Area: 7,220.0 S.F.



Drawing #: Pipe 2

Description:

&lt;--

New

--&gt;

Print Form

Dimensions Layers

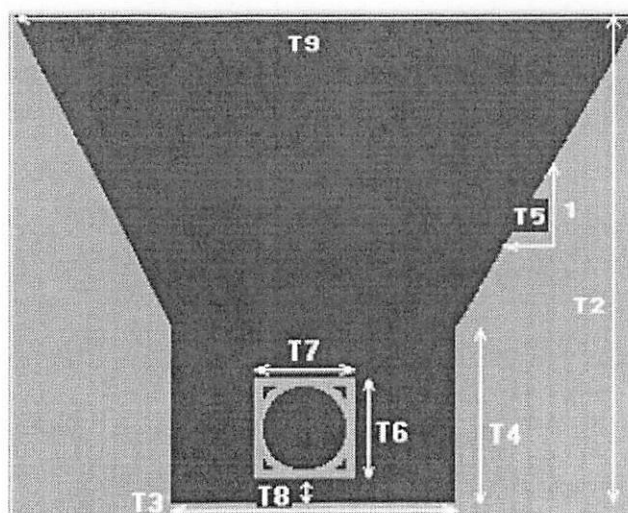
Layer 1 depth: 5.500 ft

Layer 2 depth: 0.500 ft

Layer 3 depth: 0.000 ft

Layer 4 depth: 0.000 ft

Units

☒ English☐ Metric

Neat (cy)

Waste (%)

Actual (cy)

Tonnage

Weight (tons)

Total Exc

47.833

0.000

47.833

1.000

47.833

Dirt

39.292

0.000

39.292

1.000

39.292

Base

8.542

0.000

8.542

1.000

8.542

0.000

0.000

0.000

1.000

0.000

0.000

0.000

0.000

1.000

0.000

Total Spoil

47.833

0.000

47.833

1.000

47.833



Drawing #: Pipe #3

Description:

&lt;--

New

--&gt;

Print Form

Dimensions Layers

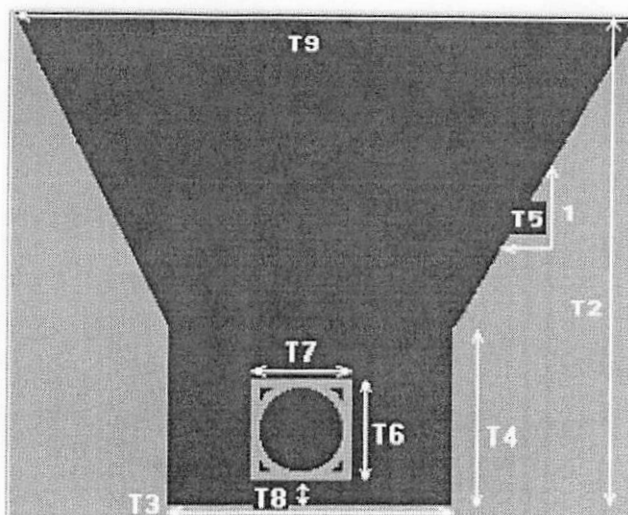
Layer 1 depth: 3.500 ft

Layer 2 depth: 0.500 ft

Layer 3 depth: 0.000 ft

Layer 4 depth: 0.000 ft

Units

☒ English☐ Metric

Neat (cy)

Waste (%)

Actual (cy)

Tonnage

Weight (tons)

|             |        |       |        |       |        |
|-------------|--------|-------|--------|-------|--------|
| Total Exc   | 26.667 | 0.000 | 26.667 | 1.000 | 26.667 |
| Dirt        | 20.556 | 0.000 | 20.556 | 1.000 | 20.556 |
| Base        | 6.111  | 0.000 | 6.111  | 1.000 | 6.111  |
|             | 0.000  | 0.000 | 0.000  | 1.000 | 0.000  |
|             | 0.000  | 0.000 | 0.000  | 1.000 | 0.000  |
| Total Spoil | 26.667 | 0.000 | 26.667 | 1.000 | 26.667 |



Drawing #: Pipe #4

Description:

<--

New

-->

Print Form

Dimensions Layers

Layer 1 depth : 4.500 ft

Layer 2 depth : 0.500 ft

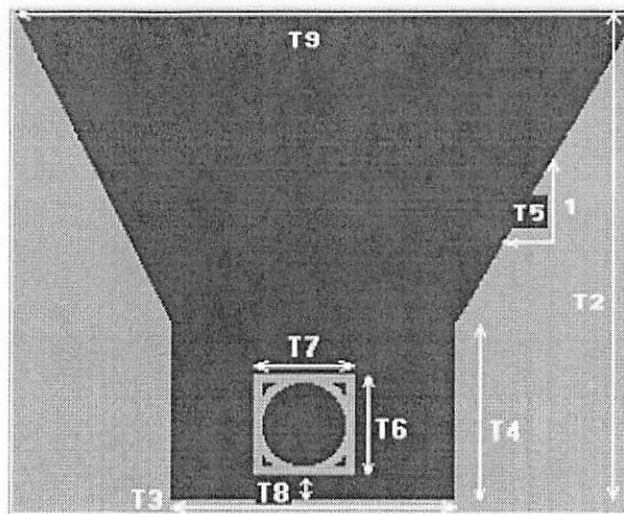
Layer 3 depth : 0.000 ft

Layer 4 depth : 0.000 ft

Units

☒ English

☐ Metric



Neat (cy)

Waste (%)

Actual (cy)

Tonnage

Weight (tons)

|             |        |       |        |       |        |
|-------------|--------|-------|--------|-------|--------|
| Total Exc   | 45.139 | 0.000 | 45.139 | 1.000 | 45.139 |
| Dirt        | 36.111 | 0.000 | 36.111 | 1.000 | 36.111 |
| Base        | 9.028  | 0.000 | 9.028  | 1.000 | 9.028  |
|             | 0.000  | 0.000 | 0.000  | 1.000 | 0.000  |
|             | 0.000  | 0.000 | 0.000  | 1.000 | 0.000  |
| Total Spoil | 45.139 | 0.000 | 45.139 | 1.000 | 0.000  |